

CEM for ammonia- and hydrogenfired power generation

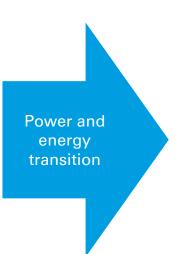
CEM 2023, Barcelona 21st September 2023

Stephen B. Harrison,
Managing Director, sbh4 consulting, Germany

Variable renewable power sources must be integrated with molecular energy storage (Power to X) and subsequent power generation (X to Power) to balance power supply and demand. Green or blue hydrogen- and ammonia-fired thermal power generation will have specific CEM challenges.









28 July 2023

Hanwha achieves almost 60% hydrogen blending on a natural gas turbine for power generation.

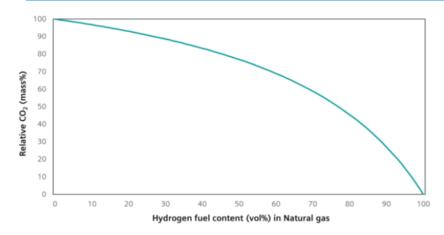




- Hanwha Impact (division of Hanwha Energy)
 - Daesan, South Korea
 - 80MWe turbine
 - 59.5% hydrogen with natural gas
 - 22% CO2 emissions reduction
 - 30% NOx emissions reduction
- South Korea has a 44% CO2 emissions reduction target by 2030
 - Nuclear power generation is threatening gas fired systems
 - Hydrogen blending is seen as a route to extend the life of gas fired turbines

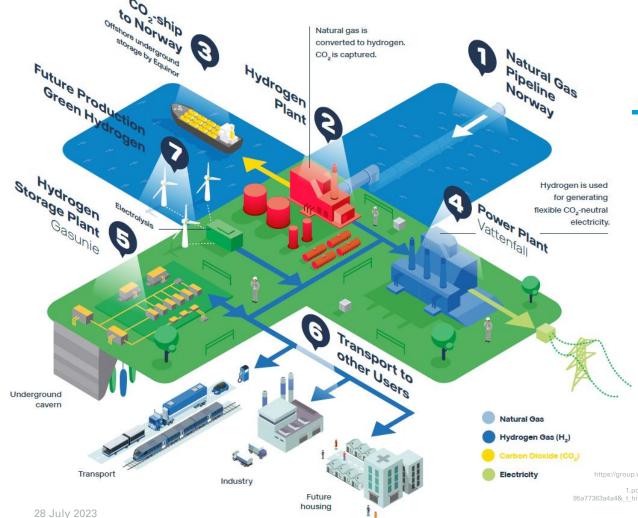
Hydrogen blending in natural gas is possible, but CO2 emissions reduction lags the H2 blend composition. Pure hydrogen must be the goal. NOx emissions reduction can be achieved with steam injection.







- A pure hydrogen flame is shorter than a methane (natural gas) flame meaning combustion happens closer to the injection zone
 - Burners must be re-designed to avoid the risk of combustion in the gas mixing chamber
 - Process control software must be re-configured to manage the flame dynamics
- The pure hydrogen flame speed and flame temperature are both higher than a methane flame meaning that NOx generation can be higher
 - Dilution with nitrogen or steam can mitigate NOx production
 - The use of steam injection is preferred and can increase power generation capacity







- Blue hydrogen production
- CCS in Utsira formation
- Long-duration Hydrogen storage in UHS salt caverns
- Hydrogen to power at RWE Magnum power plant in Eemshaven, NL (previously Vattenfall
- 1.4 GW on 3x 440MW
 Mitsubishi Power M701F
 power blocks, 100%
 hydrogen ready in 2025

https://group.vattenfall.com/nl/en/SysSiteAssets/vattenfall-nl-site-assets/wat-we-doen/onzeenergiebronnen/waterstof/vattenfall-h2m-infographic-a-

energiepromien/watternian-nzm-iniographic-a-1.pdf?_t_tags=language%3Anl%2Cstieid%3A7f0093b-3d2b-4207-8ee7-95a77363a4a4&_t_hit.id=Corporate_Web_Cms_ContentTypes_Media_PdfFile/_70931777-4936-418a-bda8--20974563178. + bit noset.

International shipping of hydrogen, hydrogen carriers and hydrogen derivatives









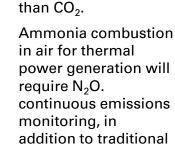






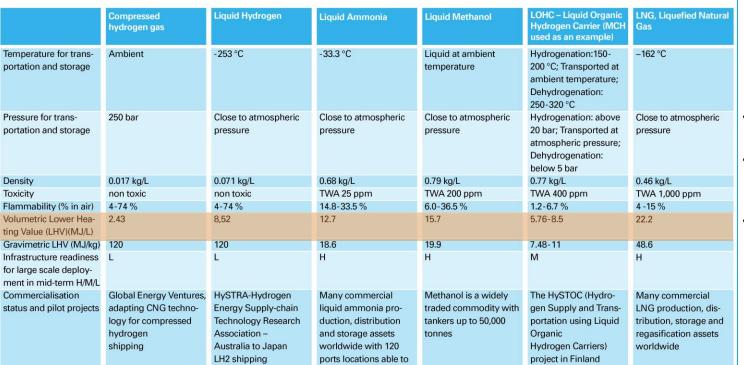






NOx measurement.

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handle ammonia



Green or blue hydrogen can be

converted to

international

ammonia to make

transportation of

Ammonia is 83%

nitrogen by mass.

N₂O emissions have a

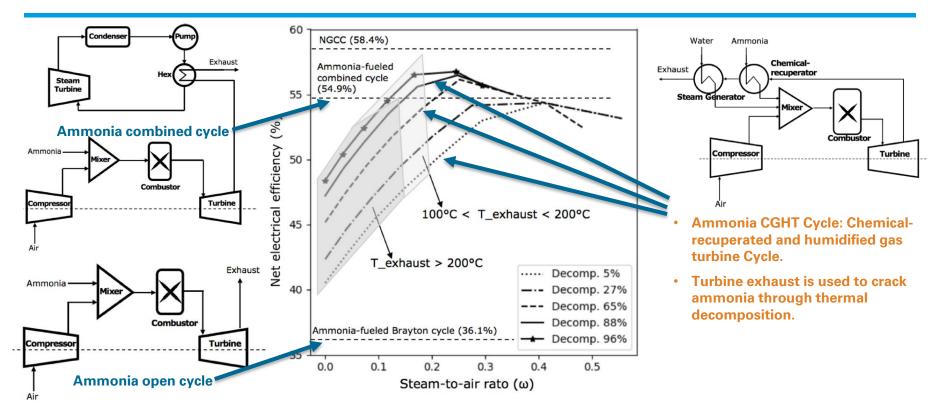
GWP circa 300 worse

clean energy vectors

more cost effective.

Ammonia in efficient power generation cycles can yield a net electrical power generation efficiency of 55% or more. Almost as good as natural gas fired IGCC at 58%.





Ammonia-fired gas turbines are in development for power generation. Ammonia combustion pathways are complex and can result in N₂O emissions. N₂O is an extremely potent GHG.





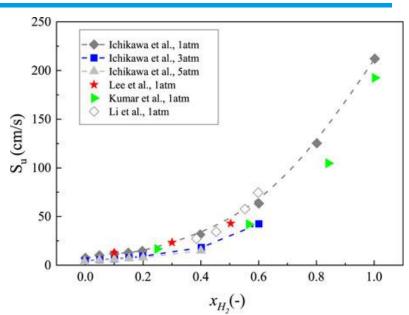
+M, +OH, +NH $+O_2$, +OH+H, +OH+OH, +H, +O+H, +OH+NO

Mitsubishi Power H-25 Series gas turbine, 40MW class

Partial cracking of ammonia to hydrogen can increase the flame speed to reduce N₂O emissions.

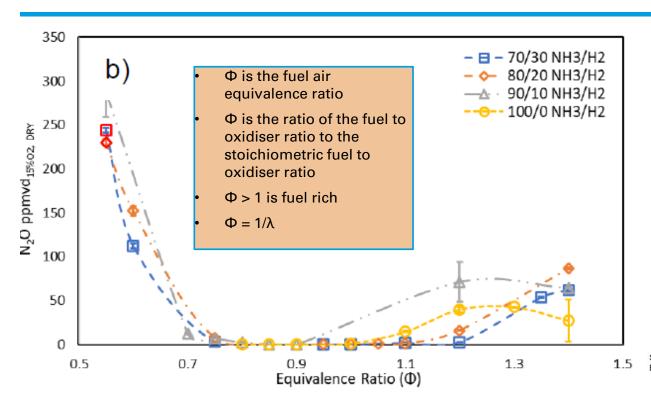


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Characteristics		Methane	Hydrogen	Ammonia
Formula		CH ₄	H ₂	NH ₃
Molecular weight	grams/mol	16	2	17
Boiling temperature	°F (°C)	-258.7 (-161.5)	-423.2 (-252.9)	-28 (-33.3)
Lower flammability limit (LFL)	%	4.4	4	15
Flame speed	cm/sec	~30-40	~200-300	~6-7
Adiabatic flame temperature	°F (°C)	~3565 (~1963)	~4000 (~2204)	~3270 (~1799)
Lower Heating value	MJ/Nm³ (BTU/scf)	35.8 (911.6)	10.8 (274.7)	14.1 (360)



In addition to cracking of ammonia to yield circa 20% to 30% hydrogen, N₂O generation can be controlled by using a stoichiometric or slightly oxygen-rich gas mix to the burner.







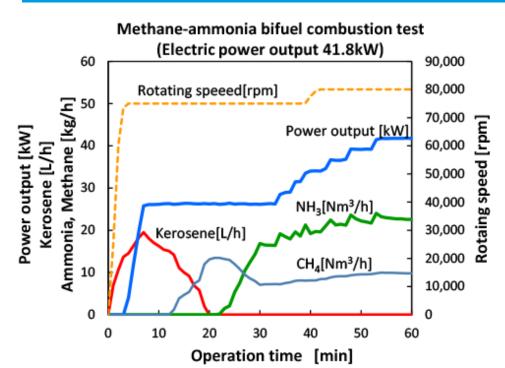
A Rosemount CT5100 QCL gas analyser was used for this 2021 paper

Nitrogen Oxides as a By-product of Ammonia/Hydrogen Combustion Regimes

Syed Mashruk^{a,*}, Marina Kovaleva^a, Cheng Tung Chong^b, Akihiro Hayakawa^c, Ekenechukwu C. Okafor^d, Agustin Valera-Medina^a

AIST in Japan has run a pilot project to co-fire ammonia with liquid fuels or natural gas on a micro gas turbine.

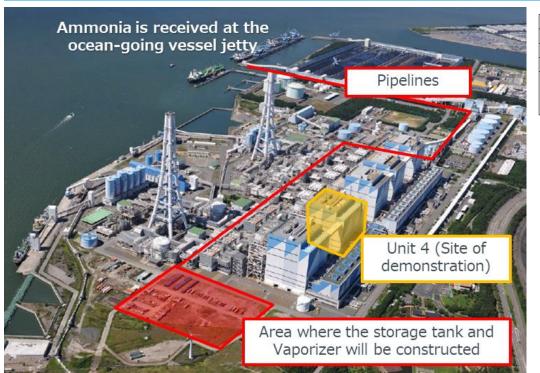






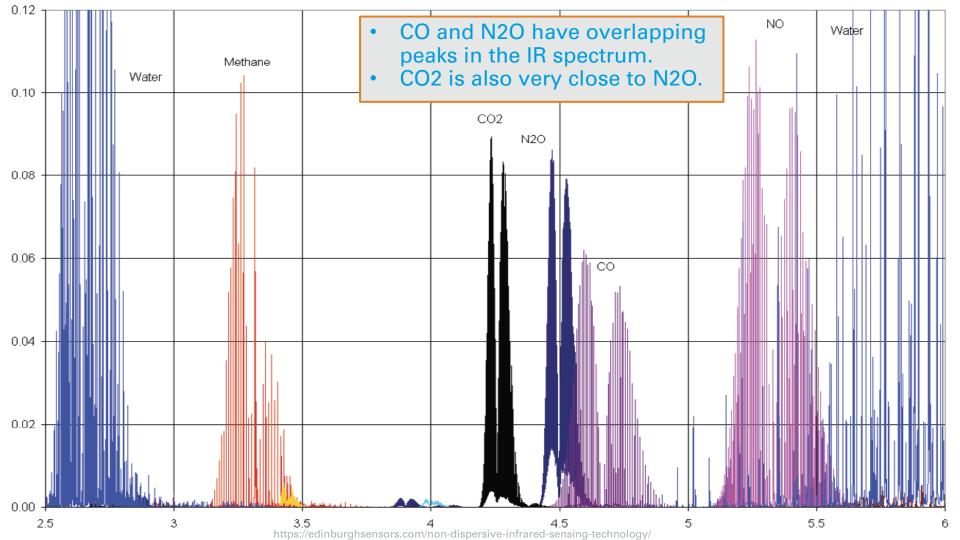
Ammonia co-firing on coal-fired power plant in Japan planned for 2024. N₂O emissions monitoring will also be required.

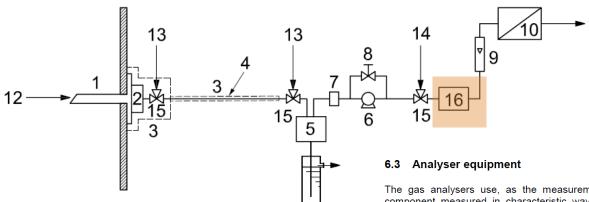




Buyer	JERA	
Supply period	Long-term contract from FY 2027 into the 2040s	
Quantity	Up to 500,000 tons per year	
Delivery mode	FOB	
Other	As a rule, CO ₂ is either not generated during ammonia production or is	
	captured and stored.	
	JERA has the opportunity to participate in production projects	

- JERA's Coal-fired Hekinan power station (4.1GWe)
- Demonstration project on unit 4 (1GWe)
- First commercial demonstration of 20% ammonia co-firing





CO must be converted to CO2 to enable accurate N2O measurement.

ISO

CO2 interference can be compensated with an additional channel in the analyser.

The gas analysers use, as the measurement principle, the absorption of infrared radiation (IR) by the component measured in characteristic wavelength ranges. The analysers operate according to the nondispersive IR method (NDIR), while the selectivity of measurement is achieved by the radiation detector which is filled with the component to be measured. A schematic diagram of a typical analyser is given in Figure A.1.

Special attention should be given to CO and CO2 interference, since for detection of N2O the absorption at around 4,5 µm is usually used, while CO has its absorption at 4,5 µm to 4,7 µm and CO₂ has its absorption at 4,3 μm. The CO interference can be excluded by using the converter (see 6.2.8). The CO₂ sensitivity requires determination with CO2 test gases. During real operation, CO2 requires simultaneous measurement to yield data for real-time correction of the N₂O readings. In many instruments, this CO₂ interference correction is done automatically through a CO₂ channel.

Since it can interfere with the measurement and lead to condensation in the analyser, water vapour present in the sampled gas is condensed in a gas cooler before the gas enters the analyser. Note that the presence of water droplets can affect the analysis of N2O, since the solubility of N2O in water is 1,2 g/l (at 20 °C, 101,3 kPa).

> INTERNATIONAL STANDARD 21258

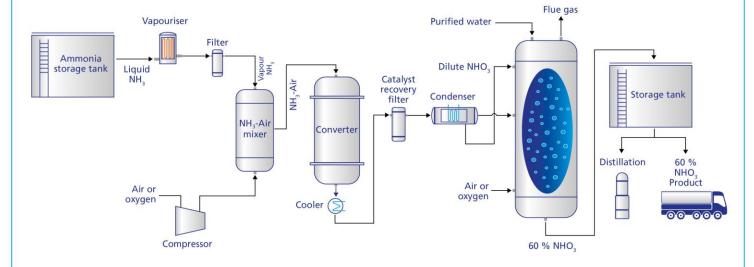
> Stationary source emissions — Determination of the mass concentration of dinitrogen monoxide (N2O) — Reference method: Non-dispersive infrared method

Key

- gas sampling probe
- primary filter
- heating (for use as necessary)
- sampling line (heated as necessary)
- sample cooler with condensate separator
- sample pump
- secondary filter
- needle valve
- flow meter
- N₂O analyser
- output
- inlet for zero and span gas (preferably in front of the nozzle) to check the complete system
- inlet for zero and span gas to check the conditioning system and N₂O analyser
- inlet for zero and span gas to check the converter and N2O analyser
- valve

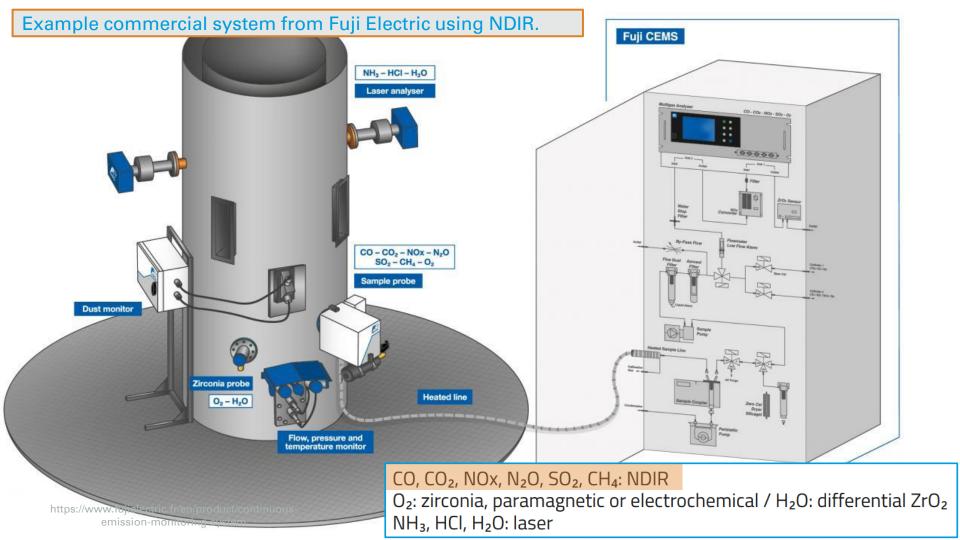
converter for CO oxidation 14

Ostwald Process for Nitric Acid Production



- As a GHG, N₂O emissions are covered in Annex I of the EU ETS Directive.
- Relevant industries are production of nitric acid, adipic acid, glyoxal and glyoxylic acid.
- N₂O emissions monitoring technologies from these sectors can be leveraged for ammonia fired power generation.

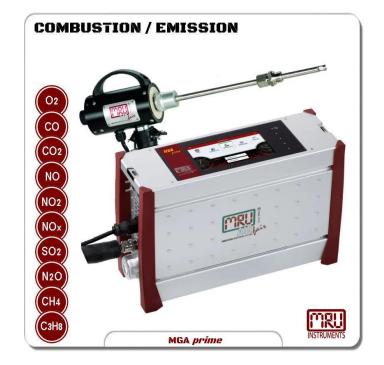




Example commercial systems from MRU using NDIR.







Example commercial system from MKS using FTIR.



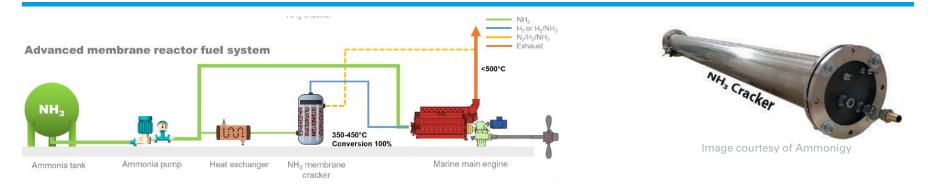
Gas Comp.	Cert. Range	Supp. Range 1	Supp. Range 2
CH ₄	0 - 15	0 - 50	0 - 500
CO	0 - 75	0 - 300	0 - 1500
HCI	0 - 15	0 - 90	0 - 200
HF	0 - 3	0 - 10	_
N ₂ O	0 - 50	0 - 100	0 - 500
NH ₃	0 - 10	0 - 75	_
NO	0 - 200	0 - 400	0 - 1500
NO ₂	0 - 50	0 - 100	0 - 1000
SO ₂	0 - 75	0 - 300	0 - 2000

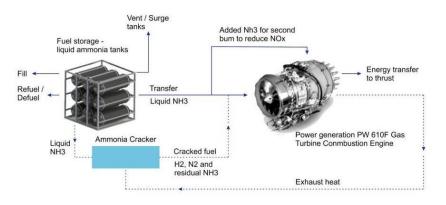
Table 1 — Gas Components and Ranges in mg/m³ Addressed by the TÜV & MCERTS certified MGS300 system. For availability of additional gases and ranges, please contact MKS for more information.



Partial cracking of ammonia can also be used in rail, maritime and aviation combustion engines. N₂O and NOx emissions reduction is a major development challenge and monitoring will be required during system testing and engine development.









sbh4 consulting



Introduction to Stephen B. Harrison

Stephen B. Harrison is the founder and managing director at sbh4 GmbH in Germany. His work focuses on decarbonisation and greenhouse gas emissions reduction. Hydrogen and CCTUS are fundamental pillars of his consulting practice, and he supports many industrial clients with their decarbonisation programmes.

Operating companies, gas analyser OEMs, private equity firms, investment fund managers and start-ups are also regular clients. Stephen has accumulated extensive M&A and investment due diligence experience in the clean-tech sector.

Stephen served as the international hydrogen and CCTUS expert for multiple World Bank, IFC and ADB projects in Namibia, Pakistan, Palau and Viet Nam. His background is in industrial and specialty gases, including 27 years at BOC Gases, The BOC Group and Linde Gas. For 14 years, he was a global business leader in these FTSE100 and DAX30 companies.

As a member of the H2 View and **gas**world editorial advisory boards, Stephen advises the direction for these leading international publications.

Stephen has served as a member of the scientific committee for CEM 2023. He also served on the Technical Committee for the Green Hydrogen Summit in Oman in December 2022 and the Advisory Board of the International Power Summit in Munich in September 2022.



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